

UTC Steering of Atomic Clocks



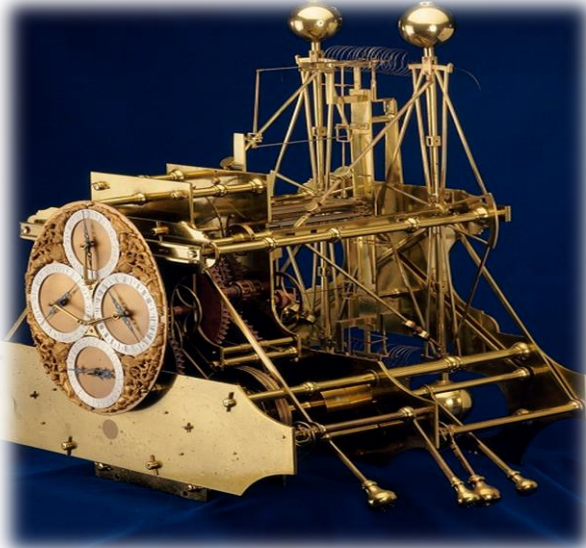
Anthony Flavin, MIET

Chronos Technology Ltd

ITSF, Prague, November 1st 2016 – Session 4

Performance improvement

- Candidate for steering



Harrison's H1



5071A Caesium H19



Caesium Fountain

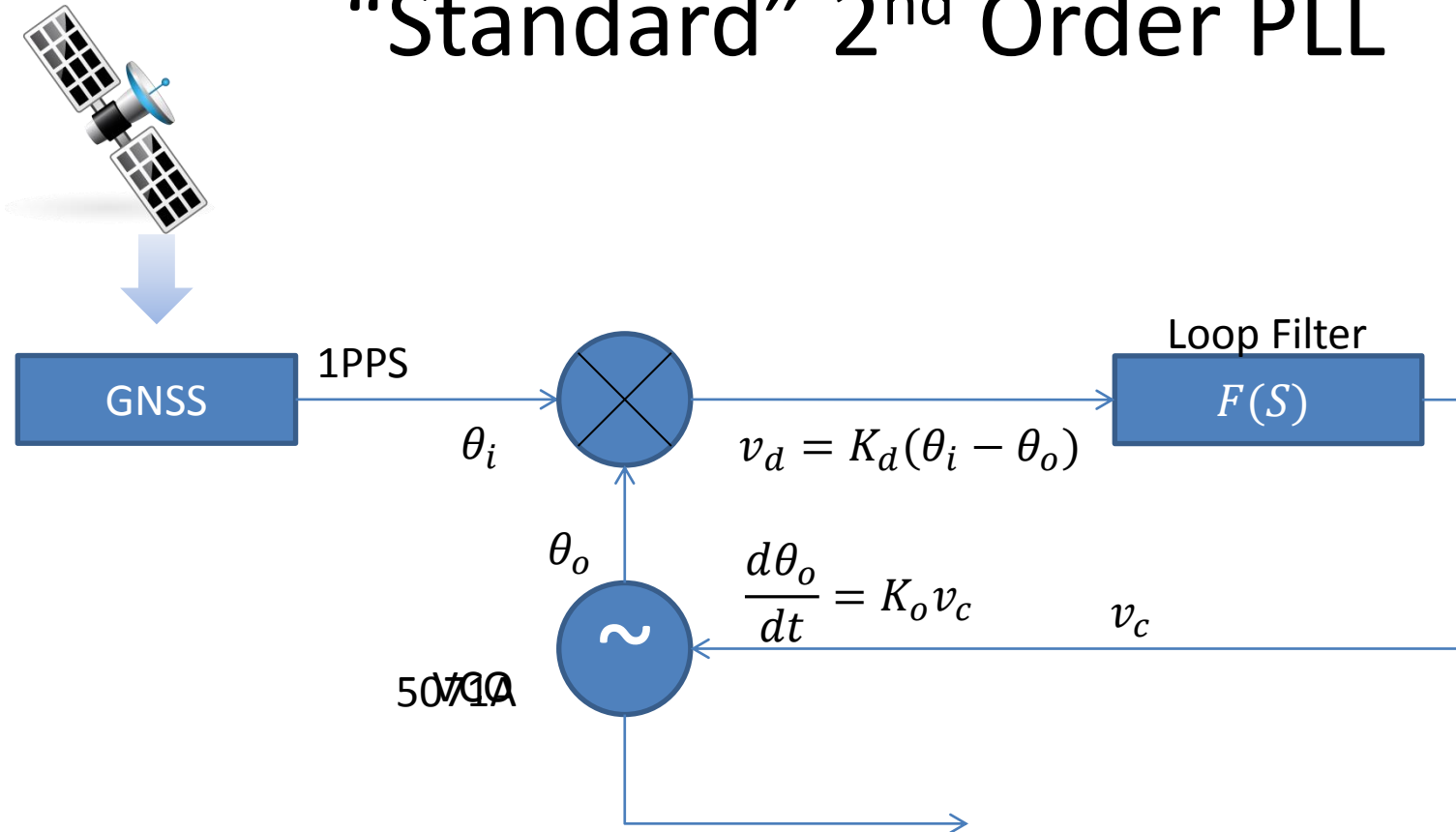
Courtesy of NPL

5071A Basic Performance



Parameter		Standard Cesium Beam Tube. Values are within:	High-performance Cesium Beam Tube (Option 001).
Accuracy†		$\pm 1 \times 10^{-12}$	$\pm 5 \times 10^{-13}$
Frequency Change vs Environment		$\pm 1 \times 10^{-13}$	$\pm 8 \times 10^{-14}$
Warm-up Time: To normal operation status (typical) To full specifications (typical)		15 minutes 30 minutes	15 minutes 30 minutes
Reproducibility†		$\pm 1.0 \times 10^{-13}$	$\pm 1.0 \times 10^{-13}$
Long-term Stability			
Time domain Stability†	Averaging Time		
5- and 10-MHz outputs	10 ⁴ seconds	$\leq 2.7 \times 10^{-13}$	$\leq 8.5 \times 10^{-14}$
	10 ⁵ seconds	$\leq 8.5 \times 10^{-14}$	$\leq 2.7 \times 10^{-14}$
	5 days	$\leq 5.0 \times 10^{-14}$	$\leq 1.0 \times 10^{-14}$
	30 days	$\leq 5.0 \times 10^{-14}$	$\leq 1.0 \times 10^{-14}$
Flicker Floor Value†	Guaranteed	$\leq 5.0 \times 10^{-14}$	$\leq 1.0 \times 10^{-14}$
	Typical††	$\leq 1.5 \times 10^{-14}$	$\leq 5.0 \times 10^{-15}$

“Standard” 2nd Order PLL

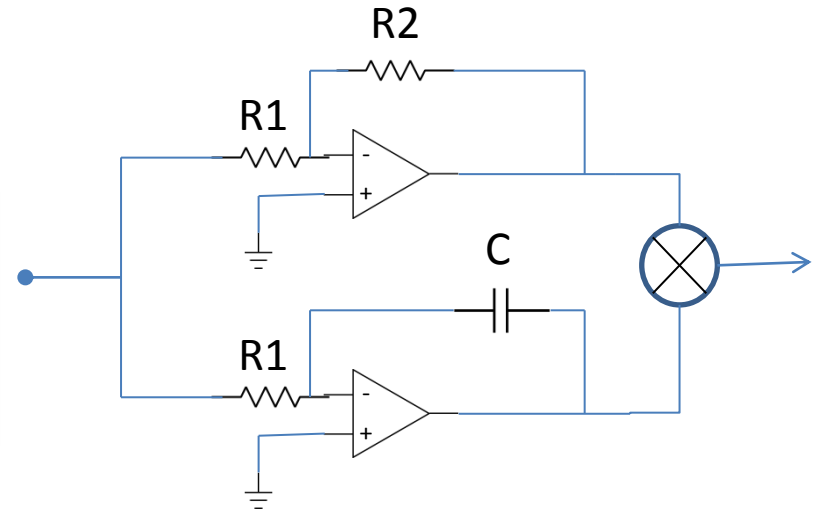
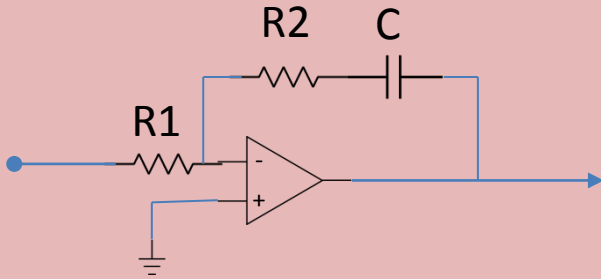


Classic Active loop filter

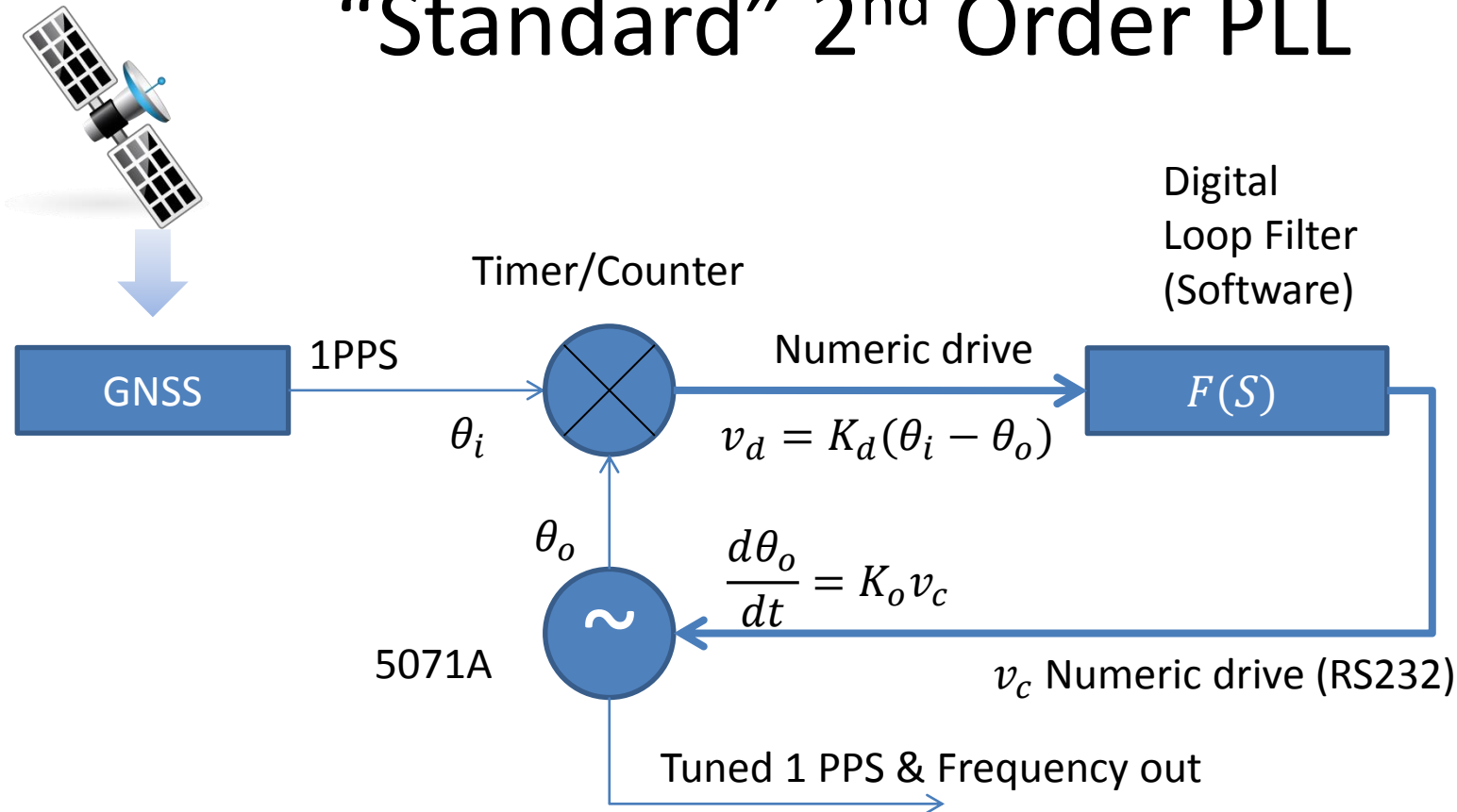
Natural frequency $\omega_n = \left(\frac{K_o K_d}{\tau_1}\right)^{1/2}$

Damping Factor $\zeta = \frac{\tau_2}{2} \left(\frac{K_o K_d}{\tau_1}\right)^{1/2} = \frac{\tau_2 \omega_n}{2}$

Where:- $\tau_1 = R_1 C$ and $\tau_2 = R_2 C$



“Standard” 2nd Order PLL



Set for 30 days settling times

Natural frequency $\omega_n = \left(\frac{K_o K_d}{\tau_1}\right)^{1/2}$

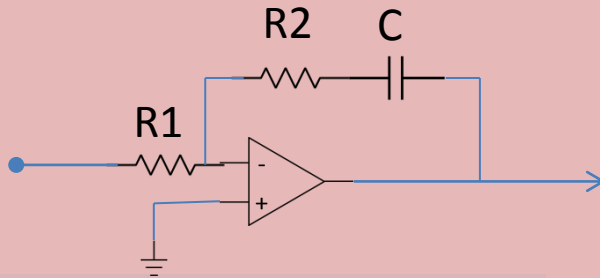
Caesium gives $k_o = 1 * 10^{-15}$

Damping Factor $\zeta = \frac{\tau_2}{2} \left(\frac{K_o K_d}{\tau_1}\right)^{1/2} = \frac{\tau_2 \omega_n}{2}$

Phase detector $k_d = 2 * \pi$

Where:- $\tau_1 = R_1 C$ and $\tau_2 = R_2 C$

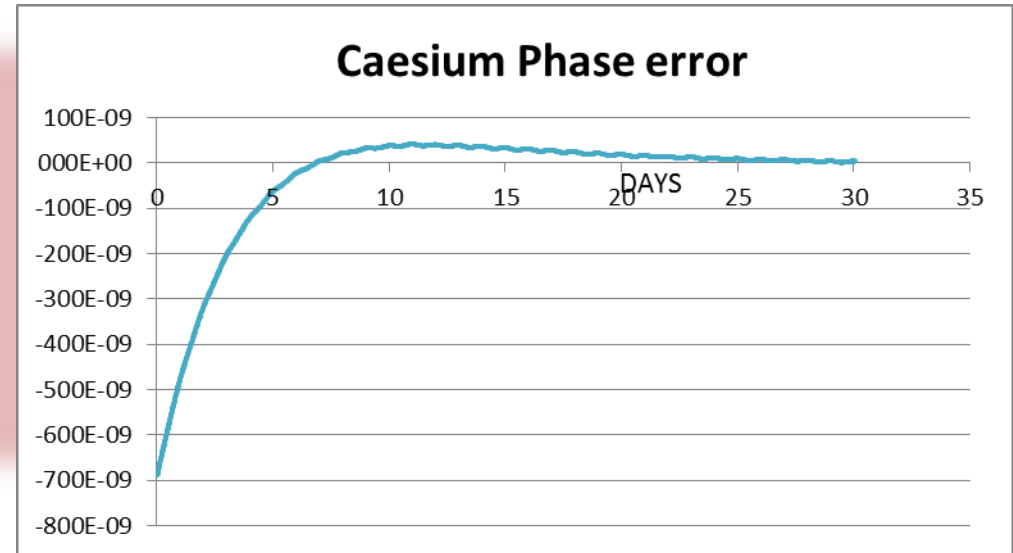
- Unrealistic test times



$R_1 = 1 \Omega$

$R_2 = 5 * 10^9 \Omega = 5000M\Omega$

$C = 1.6 F$



Pro's Cons

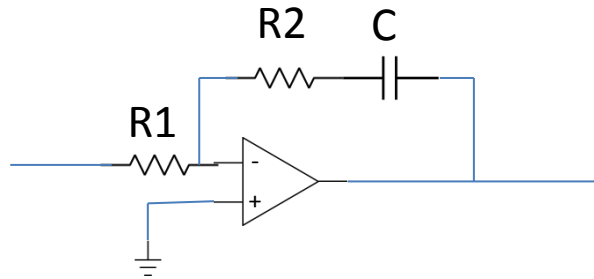
- Very good stability (Simulated)
- Caesium flicker noise dominates at output
 - $\leq 5 * 10^{-14}$
- Unrealistic development/test times
- Very long start-up times

Faster time constant

Natural frequency $\omega_n = \left(\frac{K_o K_d}{\tau_1}\right)^{1/2}$

Damping Factor $\zeta = \frac{\tau_2}{2} \left(\frac{K_o K_d}{\tau_1}\right)^{1/2} = \frac{\tau_2 \omega_n}{2}$

Where:- $\tau_1 = R_1 C$ and $\tau_2 = R_2 C$

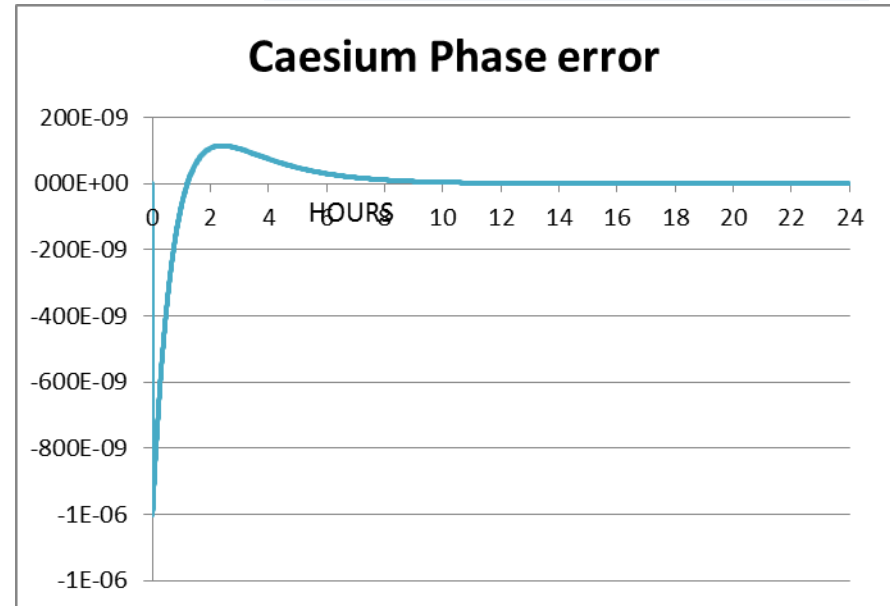


- Better test times
- Stick with this?

$R1 = 1 \Omega$

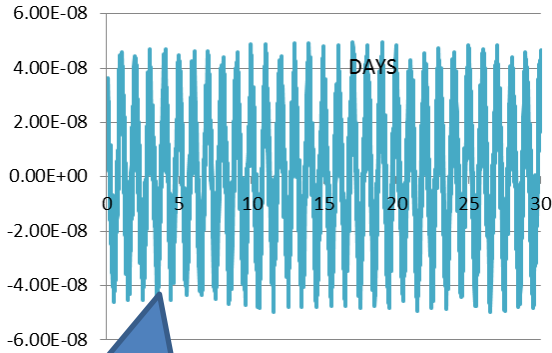
$R2 = 5 * 10^{11} \Omega$

$C = 20 \mu F$



GPS Noise

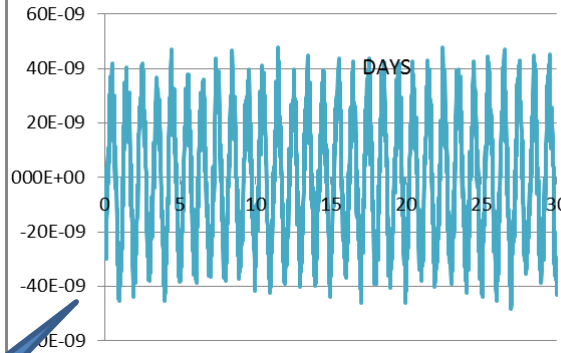
GPSNoise



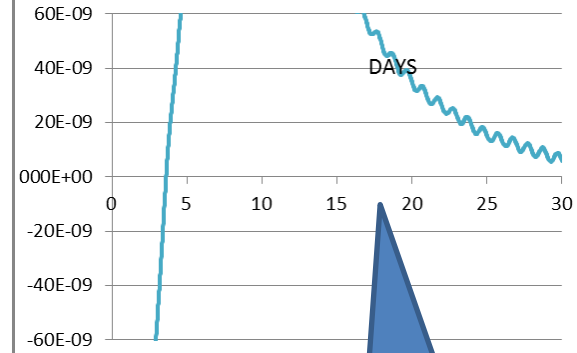
30ns P-P Diurnal
20ns P-P Random

Most noise passed through

Caesium Phase Fast Loop

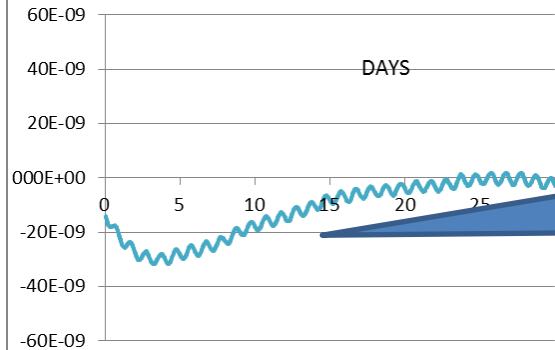


Caesium Phase Slow Loop



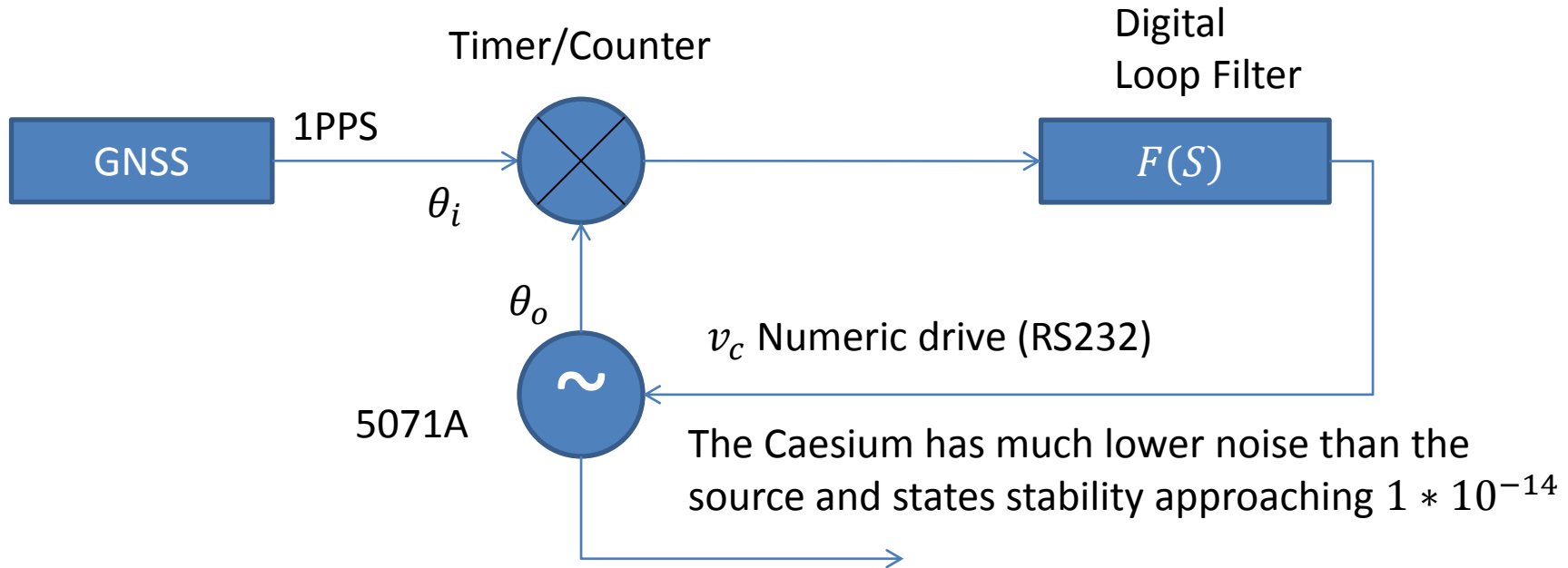
Good noise rejection but slow settling

Combined Loop



Optimal – good noise rejection – settling offset minimised

“Measuring” Performance

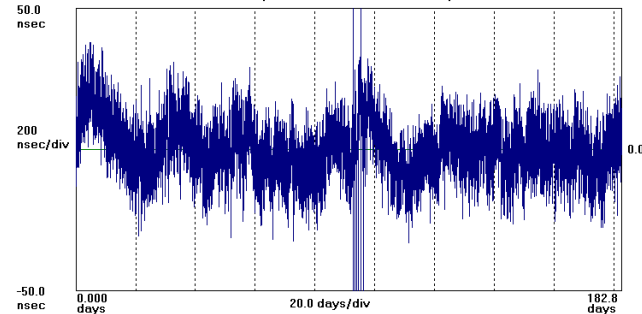


Δ We can infer phase system performance by differentiating the tuning commands.

No Hydrogen Maser required

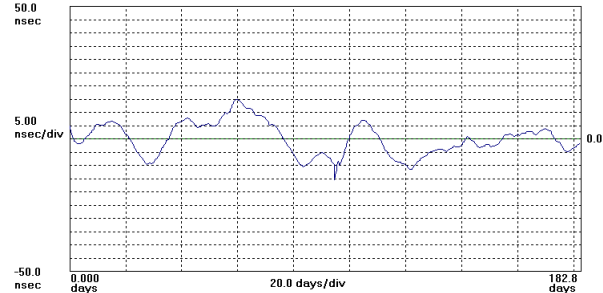
Real system results

Microsemi TimeMonitor Analyzer
 Phase deviation in units of time: Fs=16.67 MHz; Fo=2.0480000 MHz; 13-Mar-2016 15:0
 Multichannel Tester Data: Channel 1; Samples: 263174; # "Anthorn" "sample rate 60s" "--CH1-GPS 1PPS" "--CH



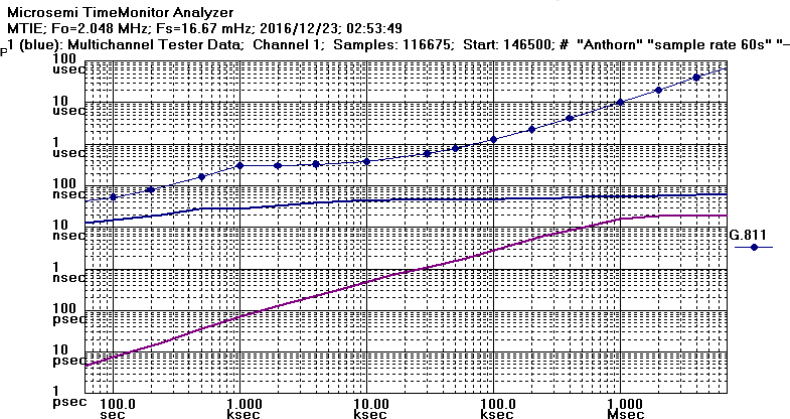
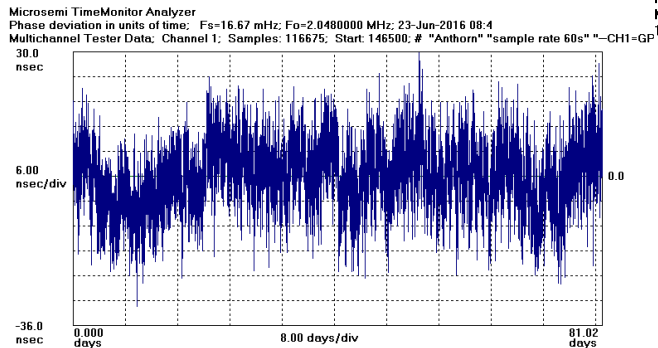
- Output from Phase detector
 - GPS Noise dominates
 - Peaks at 94 days are Space Weather event 1.5us Offsets

Microsemi TimeMonitor Analyzer
 Phase deviation in units of time: Fs=16.67 MHz; Fo=2.0480000 MHz; 13-Mar-2016 15:0
 Multichannel Tester Data: Channel 3; Samples: 263174; # "Anthorn" "sample rate 60s" "--CH1-GPS 1PPS" "--CH

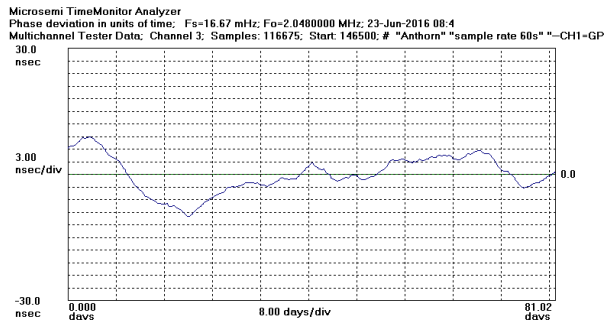


- Estimated output from Steering
 - Noise reduced to 15ns P-P

Real system results (60 days*)

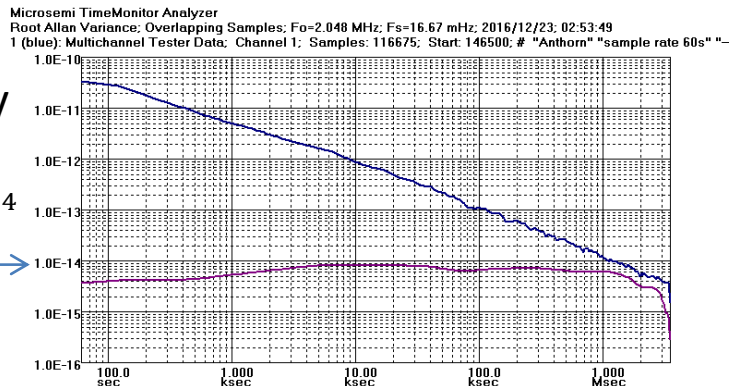


MTIE



ADEV

ADEV Below $1 * 10^{-14}$



* Last 60 days only to avoid space weather event in live data

Holdover

- What triggers Holdover
 - Source failure
 - Unusual source noise excursions
 - Space Weather (Predicted and/or Detected)
 - Planned maintenance
 - Detected Jamming/Spoofing (GNSS)
 - Can afford to be paranoid about source health

Holdover Performance

- Assuming tuned Caesium better than $5 * 10^{-14}$
 - Better than $5ns$ per day
 - Long term as per 5071A datasheet
 - Compound of tuning error + Caesium. Better than $10ns$ per day
- Return from Holdover
 - Slow response only – so up to 30 days to leak out acquired error from holdover period. After 10 days in holdover – may be worth considering restart if $100ns$ is outside of desired specification

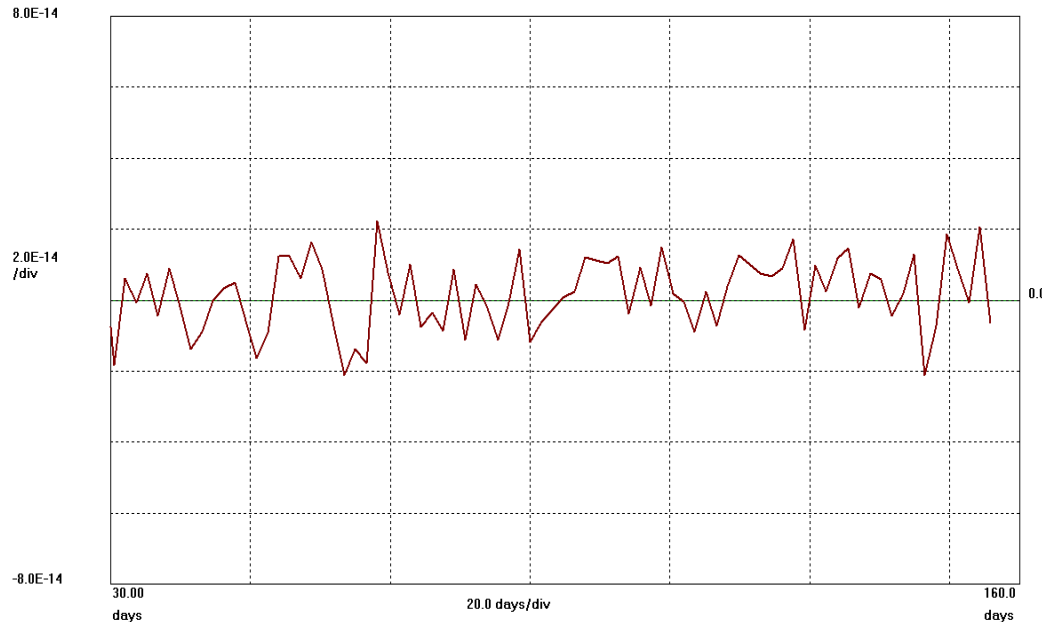
Real system results (160 days*)

Microsemi TimeMonitor Analyzer

Least square fit fractional frequency offset vs. time: N=100; 12-Apr-2016 15:0

Multichannel Tester Data; Channel 3; Samples: 225570; Start: 43200

"Anhorn" "sample rate 60s" "-CH1-GPS 1PPS" "-CH2-Anhorn RHS Caesium" "-CH3-Estimated Phase at Caesium out" "-CH4-Caesium 1PPS" "-rate=5" "-a"

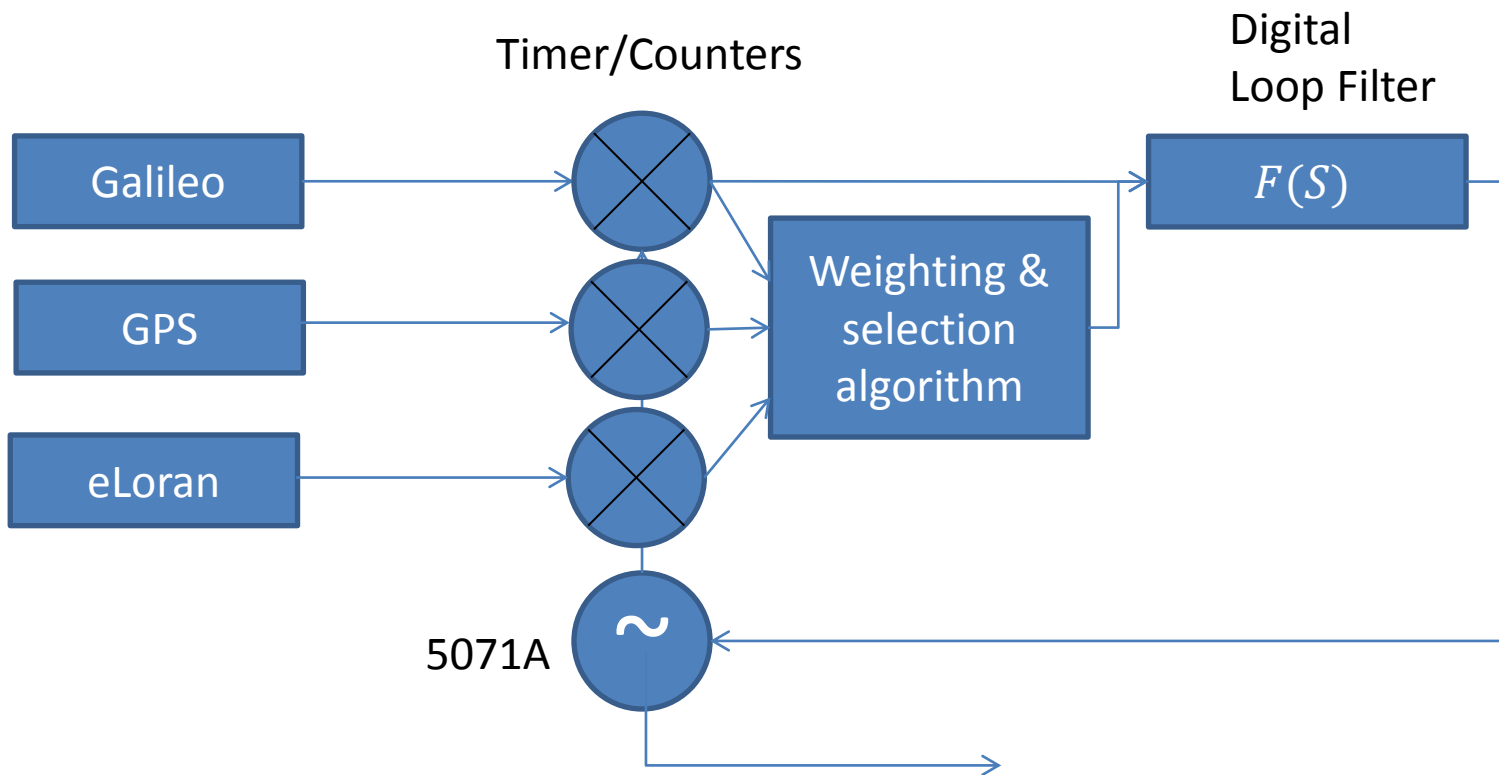


Frequency statistics

Mean	2.3E-15
Standard Error	2.8E-17
Median	2.2E-15
Mode	-1E-14
Standard Deviation	1.3E-14
Sample Variance	1.7E-28
Minimum	-3E-14
Maximum	3.7E-14
Confidence Level(95.0%)	5.4E-17

* Excludes first 30 days loop settling time

Multiple sources



Lessons

- Long time constants = Very long test/development
- Many noise sources still to be identified
 - The systems are not immune to local conditions
- Deployed systems must take account of start-up times
- Calibration difficult without a National Laboratory comparison



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